Willkommen Welcome Bienvenue



Material Aspects in Metal Additive Manufacturing Challenges, Opportunities, Visions

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Outline



- Introduction Current state of additive manufacturing of metals and alloys
- Challenges new materials for additive manufacturing
- Opportunities new materials by additive manufacturing
- Visions components from new materials with new functionalities



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Materials aspects in AM - overview



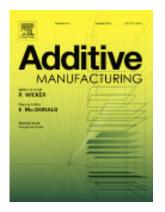
- Increasing interest in material science aspects of AM
- MS&T 2014, Pittsburgh
 - Special session «Materials science of AM»
 - 51 contributions
- TMS Annual Meeting 2015, Orlando
 - Main symposium «Additive Manufacturing»
 - 77 contributions
- MS&T 2015, Columbus
 - Main symposium «Additive Manufacturing»
 - 4 sessions, «Additive Manufacturing of Metals», «In-situ Process Monitoring, Defect Dectection and Control», «Materials Science of Additive Manufacturing», «Novel Material and Process Development for Additive Manufacturing»
 - >140 contributions
- Euromat 2015, Warzaw
 - Session: Materials Processing Additive Manufacturing

Materials aspects in AM - overview



- Journal of Materials Research, special issue September 2014 «Materials Science of additive manufacturing»
 - 34 papers on AM of metals, ceramics and polymers
- New Elsevier-journal «Additive Manufacturing»
 - "The journal covers a wide scope, comprising new technologies, processes, methods, materials, systems, and applications in the field of additive manufacturing"





The most widely used materials



- ~190 contributions to the previously mentioned conferences and journals were on metal AM (status: February 2015)
 - ~38% Ti-6Al-4V (cp-Ti)
 - ~21% Inconel 718/625
 - ~17% Stainless Steel (316L, 304)
 - ~9% Al-alloys (AlMgSi, AlCu)
 - ~8% Intermetallics (NiTi, γ-TiAl)
 - ~5% CoCrMo alloys
 - ~2% others (Mg-alloys, noble metals, composites, HEA)
- The typical title is «Microstructure and mechanical properties of Ti6Al4V/In718/SS316L produced by SLM/EBM/DMD»

Materials of interest for AM



- In Switzerland, there is a specific need for AM of the following materials
 - Advanced high-temperature alloys (γ'-hardening Ni-based alloys, Cobased alloys, TiAl) for power generation and aerospace applications
 - Tool steels, HSS, metal-superabrasives composites for advanced shape forming tools (grinding, cutting, milling etc.)
 - Precious metal alloys (Au-, Pd-, Pt-based) for jewelry and watches
 - Shape memory alloys (NiTi) for medical applications and microactuators
- → Useful information on the processability of those materials is very limited or not existing!

Parameters influencing the material properties



- The quality and the properties of AM manufactured components are strongly dependend on
 - AM processing technology (powder bed, powder feed, wire feed)
 - Energy transfer (laser, e-beam)
 - Beam shape
 - AM processing conditions (shielding gas, vacuum)
 - Scanning strategy machine type
 - Scanning parameters (P_{las}, v_{las}, hatch distance, layer thickness)
 - Alloy powder shape, grain size & size distribution
 - Powder impurities
 - Pre-heating
 - **...**
- → The correlation between the different parameters and the material properties needs to be better understood!



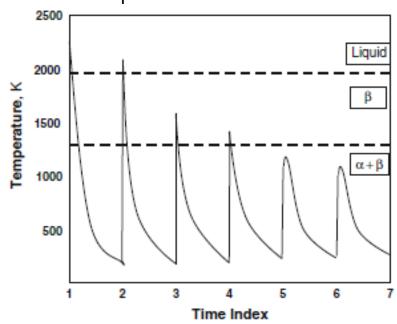
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What are the problems with AM processing of technical relevant alloys?



- Fast heating and cooling (ΔT≈10³–10⁵ K/s)
- suppressed phase transformations; supersaturated phases
- → segregation
- → hot cracking
- → thermal residual stresses
- Unidirectional heat flow into building plate/substrate
- → textured grains; anisotropic properties
- Every layer undergoes repeated heating and cooling cycles; temperatures can exceed T_{liq} or $T_{\alpha \leftrightarrow \beta}$
- → Multiple phase transformations and complex microstructures; thermal residual stresses

thermal profile of a single layer AM processed Ti-6Al-4V

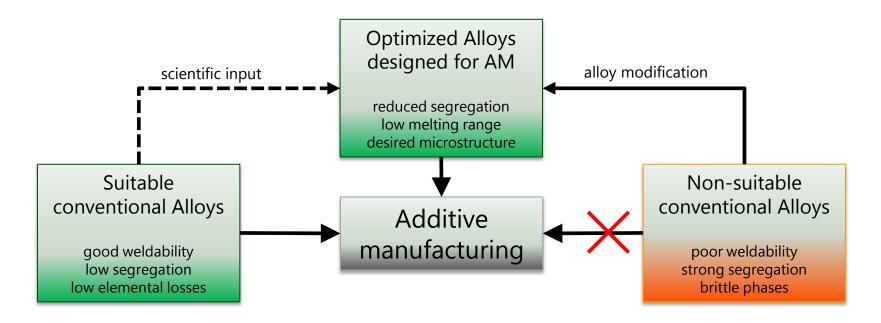


/W.E. Frazier, J. Mater. Eng. Perform. 23 (2014) 1917/

What are the problems with AM processing of technical relevant alloys?



- The phase transformations in multi-component alloys under AM conditions (=rapid solidification) must be understood and controlled!
- knowledge on stable and meta-stable phase diagrams required
- knowledge on thermodynamic and thermophysical quantities required
- knowledge on diffusion kinetics, mobilities required



Alloy development for AM – Empa approach



- Ultimate test: AM using an optimized alloy
 - AM equipment
 - new alloy according to specifications
 - suitable powder shape

processability=f(process, powder, alloy)

- Intermediate test: Alloy behavior during rapid melting and cooling using the AM equipment
 - equipment for rapid heating and cooling (=AM equipment)
 - new alloy in solid form
 - no powder needed

«processability»=f(process, alloy)

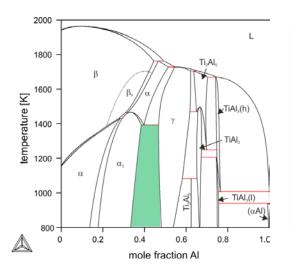
- First level test: Alloy behavior at high cooling rates
 - rapid cooling equipment (≠ AM equipment)
 - new alloy
 - no powder needed

«processability»=f(alloy)

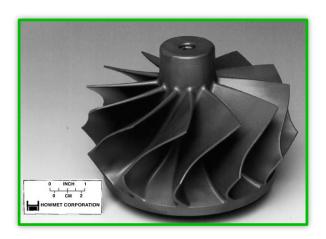
Alloy development for AM – TiAl



- Ti-Al alloys of interest for high temperature structural components
 - low density (~3.9-4.2 g/cm³)
 - high Young's modulus (~140 GPa), high strength, creep resistant
 - higher oxidation resistance than Ti alloys
 - higher service T than Ti alloys
- Fully intermetallic
 - low elongation to fracture, brittle at room temperature
 - sensitive to contamination, properties strongly dependent on phase morphology
 - Extremely difficult to process by AM

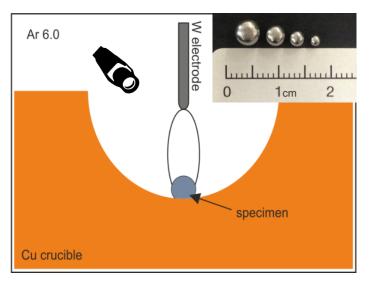


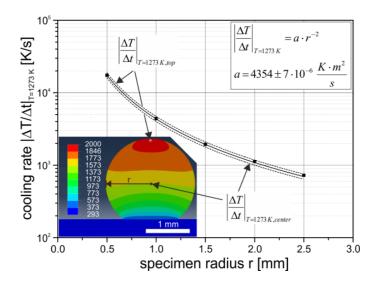




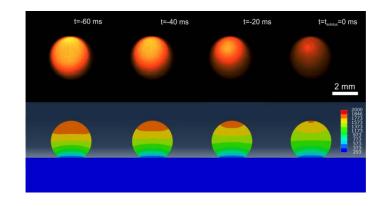
Rapid solidification – basic offline tests







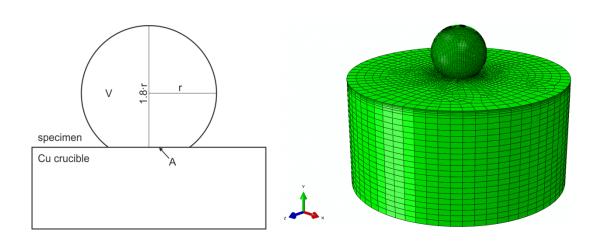
- heating and rapid solidification of small samples using W-electrode arc melting or laser beam melting
- size dependent cooling rates
 - spherical samples, the smaller the faster
 - cooling rate ~ r⁻²
- function correlating radius and cooling rate
 - single «material» parameter to describe the complete curve
- simulation verification by high speed camera measurement
 - comparable solidus propagation in experiment and simulation

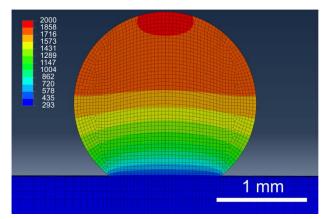


/Kenel C, Leinenbach C. J Alloys Compd 2015;637:242/

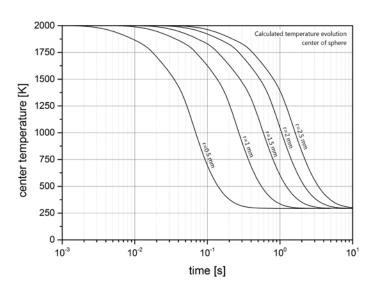
Rapid solidification – FE modeling







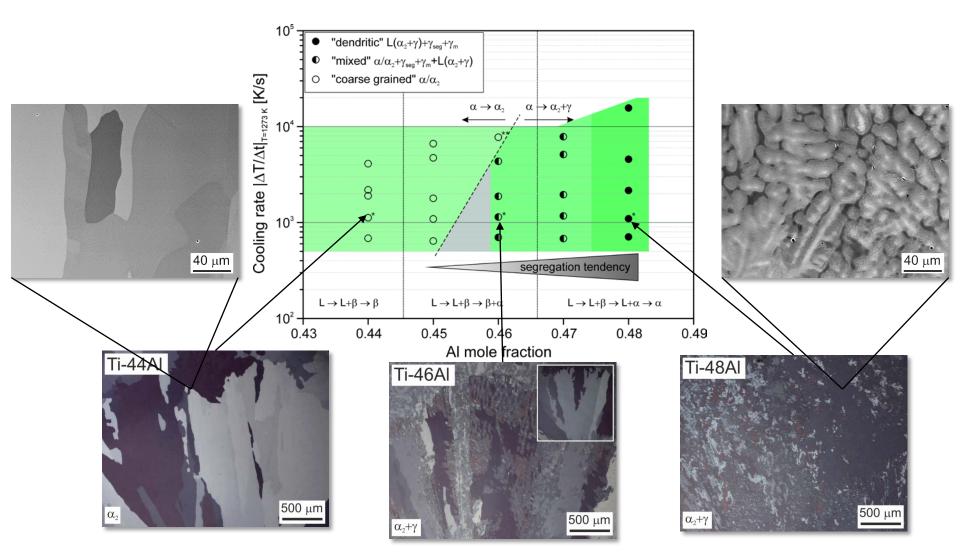
- hexahedral meshed part ~ 160'000 elements
 - 50 elements across sphere
 - dense mesh below sphere for accurate heat transport
- boundary conditions for cooled Cu part
 - side and lower surface T=293 K
- modelled heat flows
 - conductive transport sphere-substrate
 - radiation of surface to ambient surrounding
- phase transformations
 - enthalpy of fusion included for solidification



Kenel C, Leinenbach C. J Alloys Compd 2015;637:242.

Influence of cooling rate on microstructure formation

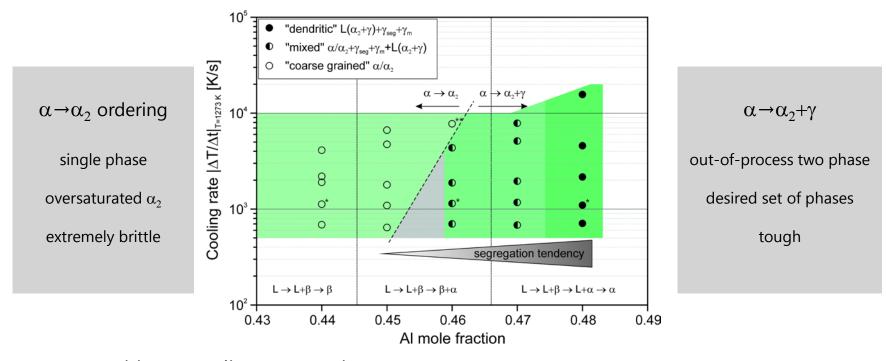




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Influence of cooling rate on microstructure formation



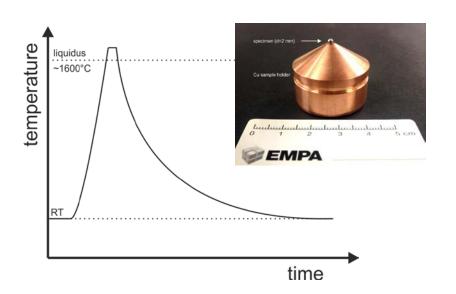


- composition cooling rate microstructure maps
 - properties relevant to processing (here: formation of intermetallic phases)
 - data for alloy selection
 - similar to processing window determination experiments → indications for suitable processing parameters
- predictability based on equilibrium phase diagram information: limited

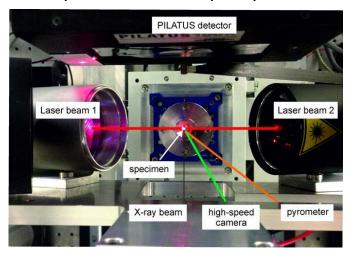
In situ Synchrotron XRD on rapidly heated and cooled alloys



(with J. Fife, H. Van Swygenhoven, D. Grolimund, S. Van Petegem – Paul-Scherrer-Institute, Villigen, CH)



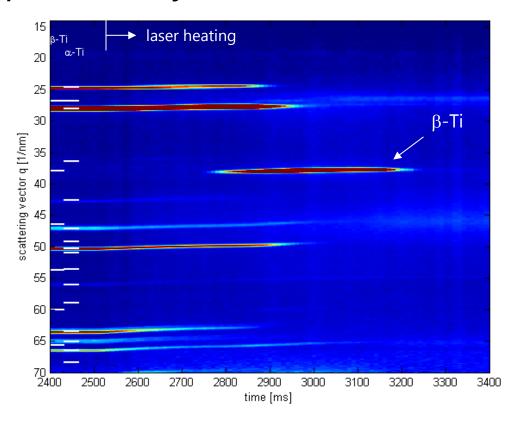
experimental setup, top view



- setup of laser beam heating stage inside Synchrotron beam line at PSI
- in situ XRD during laser melting and soldification of Ti alloys
- feasability for controlled Ti- and TiAl melting and solidification
- high speed camera measurements for additional information

In situ XRD on rapidly heated and cooled alloys – preliminary results

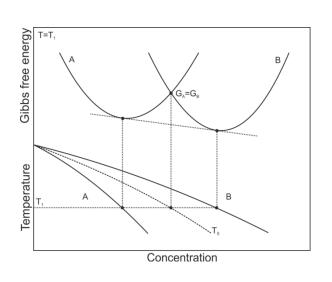


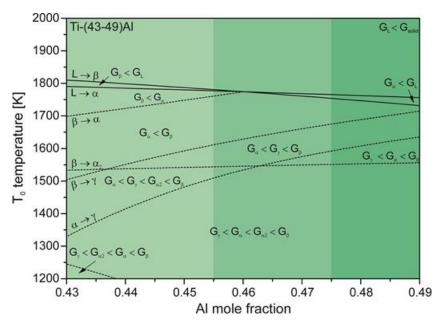


- in situ (Laue) XRD during laser melting and solidification of Ti
- $\alpha \rightarrow \beta$ phase transformation and melting clearly observable
- high temporal resolution can be reached using synchrotron radiation
- facility can be used in other beamlines (e.g. tomography)

Development of phase selection hierarchy maps



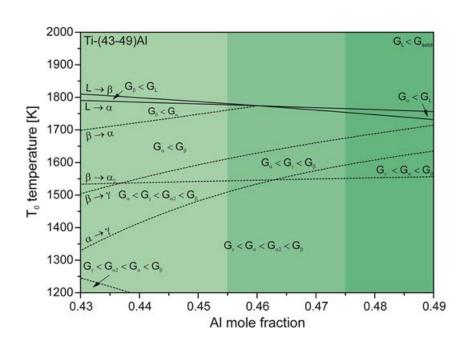


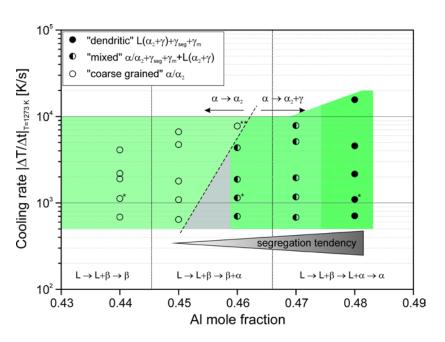


- diffusion-less phase transformation
 - ideally no diffusion → all phases have the same composition
 - phase B transforms to A if $G_A < G_B$
- T₀ temperatures for different phase transformations and solidification
 - calculated using CALPHAD
 - based on published thermodynamic assessment for Ti-Al [1]
- map constituents
 - T₀ temperature curves for specific phase transformations
 - fields with a hierarchy according to the Gibb's free energy
- «phase diagram without diffusion»

Prediction of transformation behavior





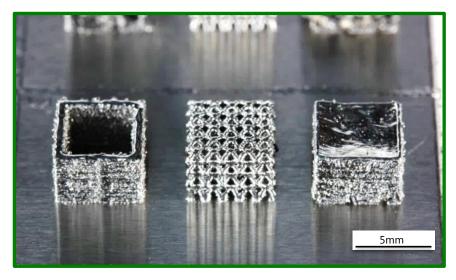


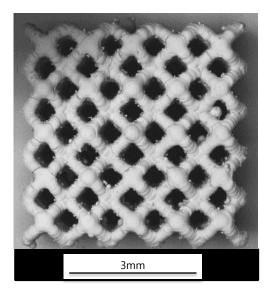
- diffusion-less T₀ concept allows to predict the changed solidification behavior
- deviation from equilibrium phase diagram can be explained
- influence of kinetics for Ti-46Al at studied cooling rate
- complementary tool for alloy development
 - pre-screening of alloys
 - understanding of experimental results
 - reduction of experimental effort

AM of TiAl with more complex geometries





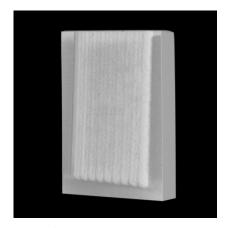




SLM 3D test structures (in collaboration with Inspire)



LMD test structure Ti-Al alloy (with TWI Ltd.)



CT of a LMD test specimen

note: structures were made from an Y₂O₃-ODS-variant







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New materials by AM



- Advantages of selective laser or electron beam melting
 - Short matter-beam interaction time due to high scanning speed
 - Small meltpool
 - High heating and cooling rates
- Very fast material consolidation
- Potential for processing of metastable materials, novel types of metalmatrix composites, or multi-material structures
 - Metal-diamond/metal-cBN composites
 - Novel High-entropy alloy components
 - **...**

New materials by AM - metal-diamond composites



(with A.B. Spierings, K. Wegener – Inspire/ETHZ)

- Metal-diamond composites interesting for high-performance cutting or grinding tools
- Conventional production: Galvanic Ni-bonding of diamond particles
 - Only single layer diamond tools possible, typically with simple geometry
- AM offers possibility to produce complexely shape geometries (e.g. internal cooling chanels
- Problem: Graphitization tendency of diamond particles at elevated temperatures
 - Depending on atmosphere (Inert atmosphere / vacuum $\approx 1'500^{\circ}$, Air $\approx 1'000^{\circ}$ C)





Approach: Brazing alloy as matrix material

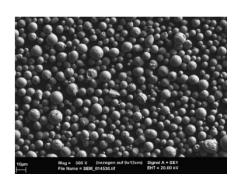


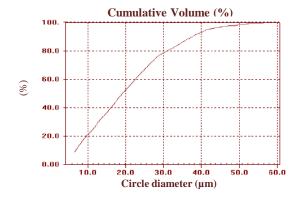
Matrix material

Cu-based active brazing alloy

- Composition
 Cu
 Sn
 Ti
 Zr

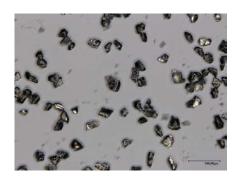
 wt. %
 73.9
 14.4
 10.2
 1.5
- High thermal conductivity (> ≈ 55 W/mK)
- $T_{\text{liquidus}} = 925^{\circ}\text{C}$
- Powder with
 - $D_{10} = 7.6 \mu m$
 - $D_{50} = 20 \mu m$
 - $D_{90} = 38 \mu m$

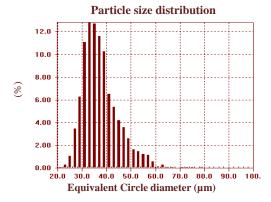




Diamond particles

- 50 vol% Ni-coated to protect the diamond particles from graphitization (additional heat sink)
- Particles
 - Mean particle Ø 33.9 ± 6.4µm

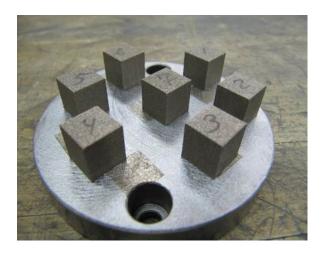






Metal-diamond composites

- SLM processing of a of brazing alloy & diamond particles
 - Stable specimens with good surface quality can be produced





SLM-samples of Diabraze with 10 vol% diamond (left) and 20 vol% Ni-coated diamond (right)

They are difficult to remove from the base plate.

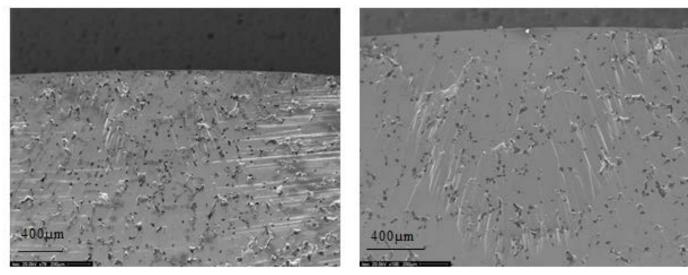
... and have already a very good abrasive effect!



Metal-diamond composites

SLM processing of a of brazing alloy & diamond particles

<u>Ion cross-section milled SEM pictures</u> of samples with 10 vol-% diamond particles



SEM (SE) - Micrographs of SLM-samples of Diabraze with 10 vol% Ni-coated diamond, energy input EL = $40.4 \, ^{J}/_{mm}3$ (left) and EL = $50.5 \, ^{J}/_{mm}3$ (right).

- Diamonds are homogeneously distributed in the matrix
- Diamonds survived almost unchanged
- Some remaining porosity and cracks are visible

Metal-diamond composites

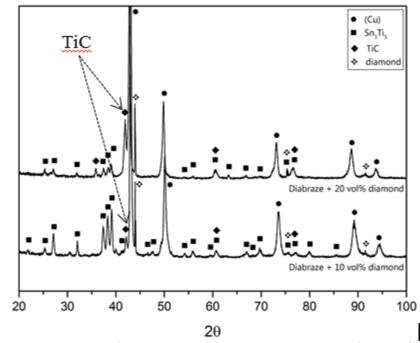


XRD spectra

- The matrix consists of a mixture of a Cu solid solution and (Cu,Sn)₃Ti₅ with Cu as the main phase.
- Formation of TiC is more pronounced for the 20 vol-% samples than for the 10 vol-% samples

Intensity a.u.

- Ni fully dissolves in the matrix (Ni peak below treshold-level of XRD).
 - → Ni was detected by EDX.



XRD-spectra of Diabraze with 10 vol% Diamond (bottom) and 20 vol% Diamond (top). The identified phases are indicated.



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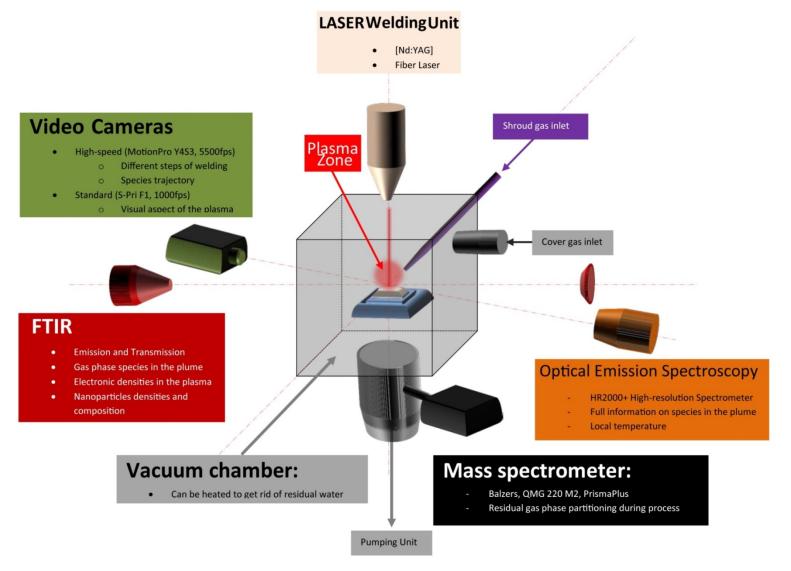
Visions



- In theory, AM allows for the fabrication of multi-material components and build-ups with complex geometries and new functionalities
 - Materials with integrated sensing capabilities (e.g. optical fibre gratings)
 - Graded structures with altered mechanical and physical properties
 - Repair of complexely shaped strcutures from composite materials
 - **...**
- Besides a thorough understanding of the materials, this requires a new level of process control
 - Local variation of laser power, scanning speed...
 - Pre-/post-heating to adjust cooling rates
 - **...**
- A control of the process requires a reliable online monitoring of the process
 - Melt pool geometries
 - Local temperatures
 - Effective laser power
 - **...**

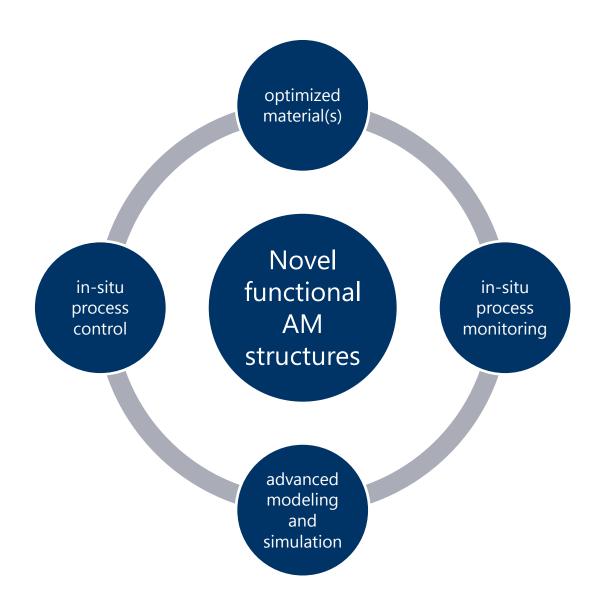
Set-up for in-situ monitoring of laser processing





The dream









Thank you

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